



Image Credit: Endurosat 12U CubeSat Platform and Chassis Image

Analytical Cost-Optimization of Orbital Parameters and Propulsion Solutions for SPS in LEO

TEXAS SSPS



The University of Texas at Austin
**Aerospace Engineering
and Engineering Mechanics**
Cockrell School of Engineering

Undergraduates



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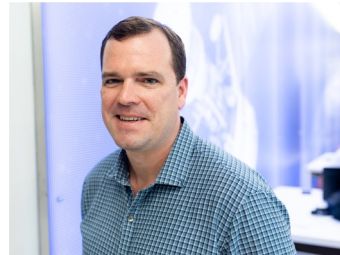


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Agenda Overview

- Introduction
- Problem and Mission
- Methods and Analysis
- Economic Results
- Conclusion

Problem and Mission

Background

Space solar power has been considered *technically feasible* since the 1970s, provided sufficient technological development in **key areas**:

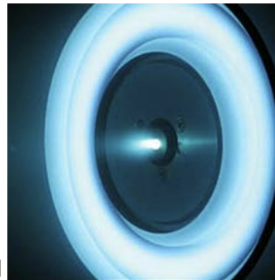
- In-space large structure assembly
- High-efficiency solar energy conversion devices (photovoltaics, batteries, etc.)
- Super-heavy reusable launch vehicles

There is a **select amount** of data on the economic merit of performance parameters. This project focuses on analysis of the following **design parameters**:

Orbital Configuration

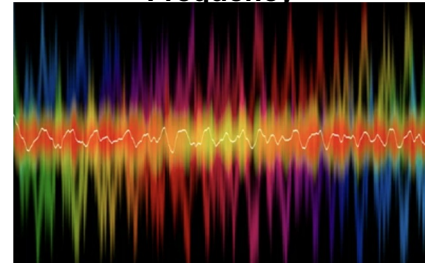


Propulsion System



[1]

**Power Transmission
Frequency**



Mission Objective

For a Solar Power Satellite (SPS) in Low Earth Orbit (LEO), we shall identify the most **economical** approach considering tradeoffs between:

**Orbital
Configurations**

**Power
Transmission
Frequency**

Propulsion Systems

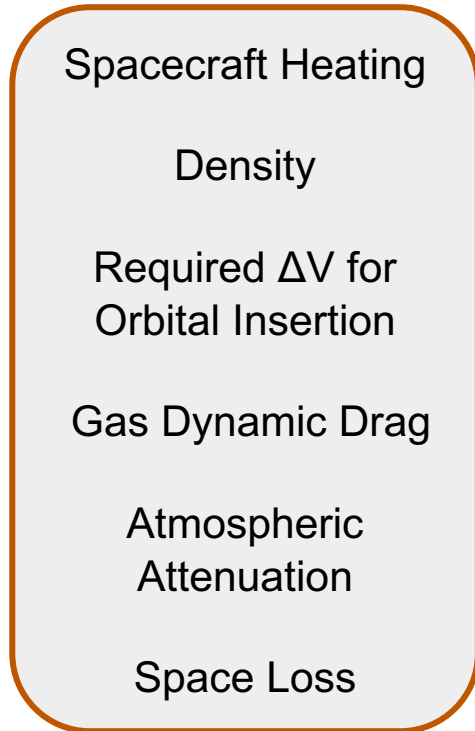


Figure 1: Conceptual image of a solar power transmission satellite

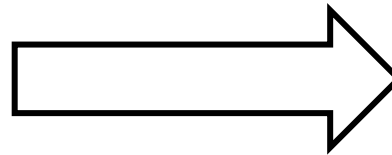
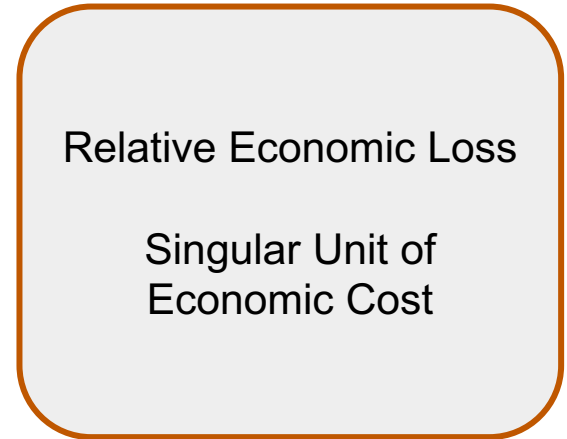
Methods and Analysis

Cost Optimized Orbit Analysis Approach

Performance Parameters



Output

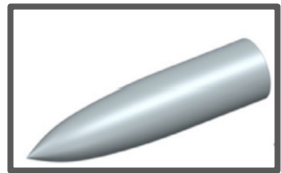


Physical models
and Economic
Estimates

Preliminary Assumptions

Drag Calculation

- Spacecraft Frontal Area: 5, 25, and 125 m²
- Mission duration: 50 years
- Launch Vehicle: SpaceX Falcon 9 (\$2000/kg to LEO)
- Retail price of energy delivered: \$0.23/kWh
- Coefficient of drag, $C_D = 2.0$



- Surface emissivity = 0.92 (Z93 coating)
- Accommodation coefficient, $\alpha = 0.05$
- Dispersive collision fraction, $g = 0.05$

Power Attenuation Calculation

- Antenna efficiency = 55%
- Altitude-averaged atmospheric thermodynamic parameters
 - Temperature = -44.2 °C,
 - Water vapor density = 0.15 g/m³
- Domain of analysis:
 - Frequency: [0, 50] GHz
 - Receiver Aperture Area: [0, 100] km²
 - Altitude: [100, 2000] km

Figure 2: Streamlined Spacecraft Body Assumption [17]

Physical Model: Density and Drag Calculation

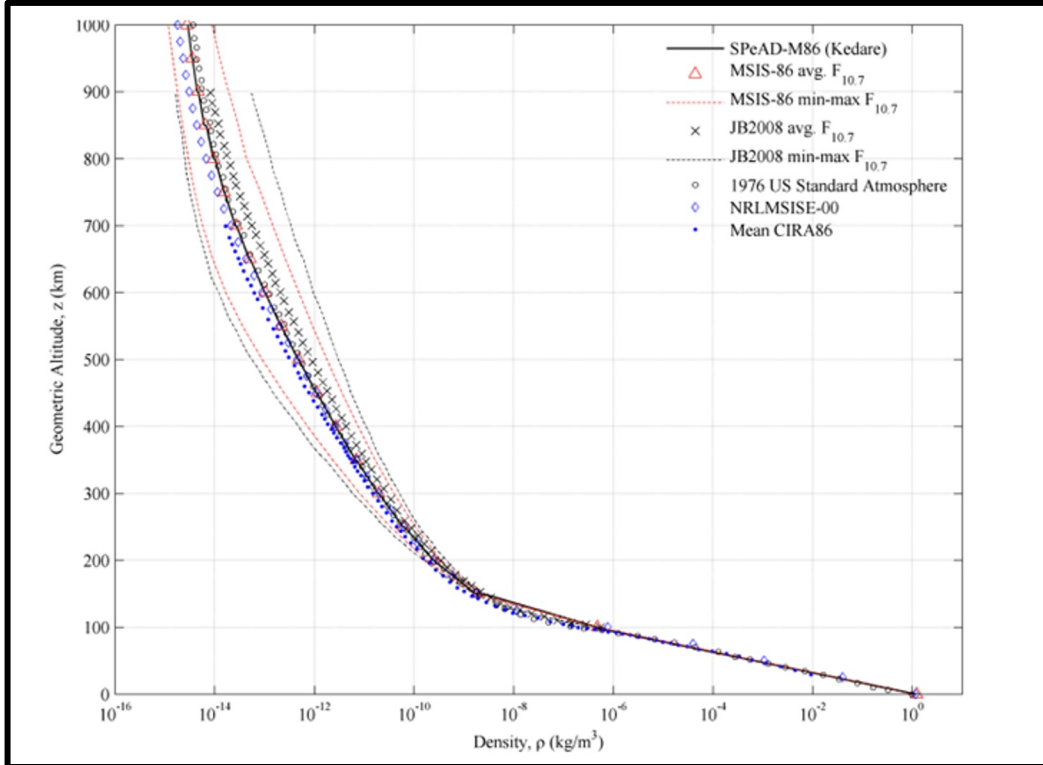


Figure 3

$$ma_{x,aero} = -\frac{1}{2} \rho V_R^2 A_{ref} C_X(\alpha, \beta, S, \sigma, T_w)$$

ρ_∞ = freestream density, u_∞ = freestream gas speed

h_0 = stagnation enthalpy, h = enthalpy

ϵ_r = spacecraft reflectivity

σ_{SB} = Stefan-Boltzmann constant

Relating Drag to Propulsive Requirements

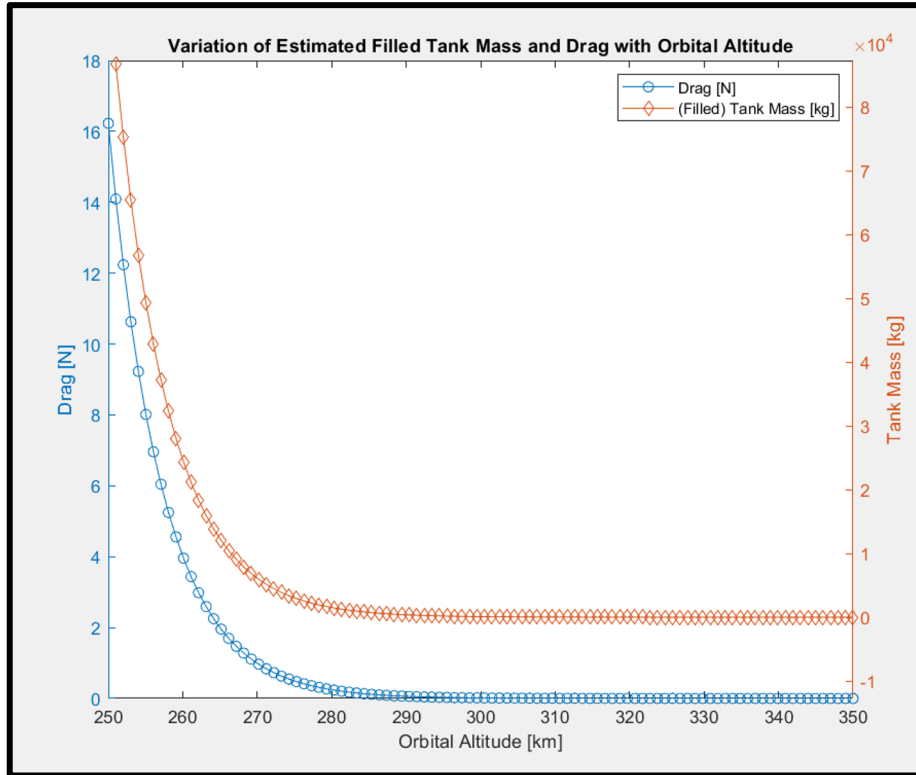


Figure 4

The following ideal gas rocket sizing equations were used for Xenon storage as a compressed gas (150 bar, 300K):

$$M_{tank} = \rho_w \cdot V_{tank}$$

$$= \rho_w \cdot (4\pi R^2 \cdot t)$$

$$t = \frac{R \cdot P_{G0}}{2 \cdot \sigma_{allow}}$$

$$R = \left(\frac{1}{4} \cdot V_{gas} \right)^{1/3}$$

M_t = tank mass

ρ_w = tank wall density

t = tank wall thickness

P_{G0} = Initial tank internal Pressure

V = Volume

Physical Model: Launch Cost

Assumptions:

- This model calculates the launch cost as a function of altitude and eccentricity
- Keplerian orbital mechanics.
- The initial orbit is a circular orbit of 100 km altitude ($\Delta v \sim 8$ km/s).
- 'Cost per Δv ': $\sim \$1000$ per 1 m/s (from SpaceX Falcon 9 payload to LEO launch cost) [3]

$$\Delta v \approx \sqrt{\left(\frac{2\mu}{r_i}\right) - \left(\frac{\mu}{r_f}\right)}$$

μ = gravitational parameter
 r_i = initial radius at apogee
 r_f = final radius at apogee
 v = spacecraft speed

Physical Model: Atmospheric Attenuation & Space Loss

- Atmospheric Attenuation calculated using:
 - International Telecommunication Union (ITU-R P.676-10)

- Free Space Path Loss calculated using:
$$FSPL(dB) = 20 \log_{10}(d) + 20 \log_{10}(f) + 92.45$$

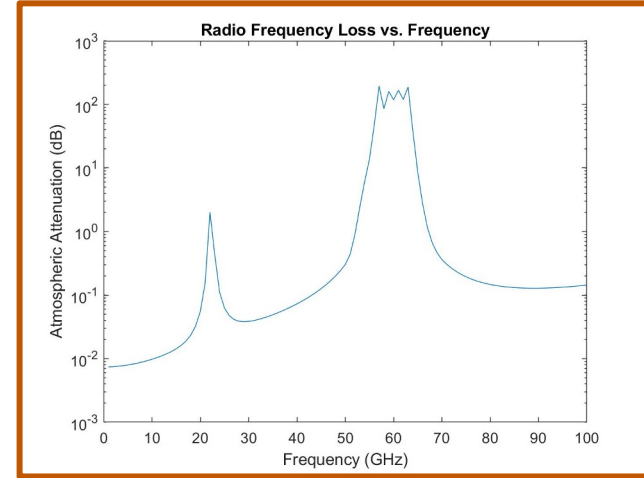


Figure 5:

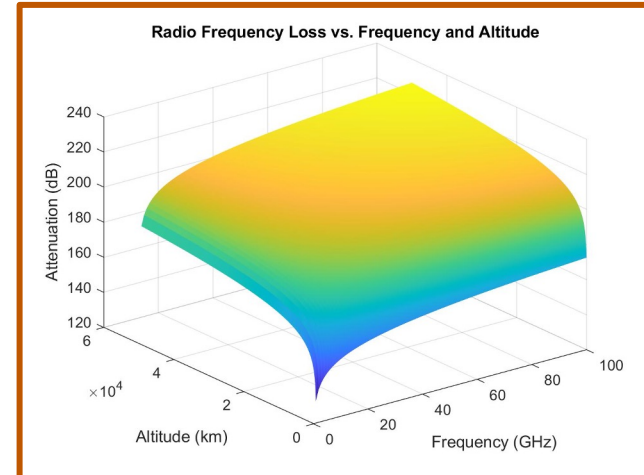


Figure 6:

Cost-Optimized Frequency

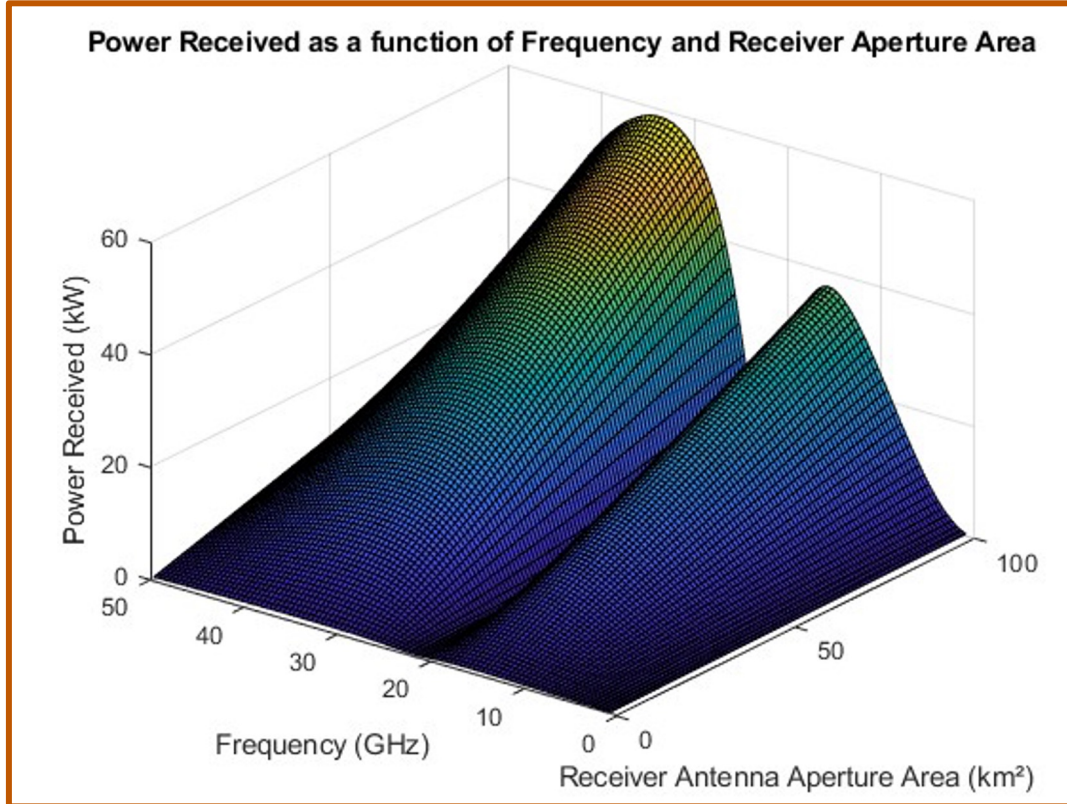


Figure 7

- Current technology with high efficiencies exist currently under 50 GHz.
- The optimal frequency is **33.67 GHz**.
- A secondary peak occurs at **15.78 GHz**.

$$G_{db} = 10 \log_{10} \left(\frac{4\pi\eta A}{\lambda^2} \right)$$

Eq: Antenna Gain

[9]

Economic Results

Performance Data to Economics

A **Monte Carlo analysis** was used to quantify the economic merit associated with the following physical parameters for 15,000 orbital configurations for a space-based solar power system.

SpaceCraft Heating

Density

Required Delta V for
Orbital Insertion

Gas Dynamic Drag

Atmospheric
Attenuation

Space Loss



\$2000/kg for orbital
insertion

\$0.23/kWh price of
energy



Economic merit of
**orbital
configuration &
power
transmission
frequency**

Legend

- 125 m² frontal area
- 5 m² frontal area

Results - Mission Cost

Total Mission Cost as a Function of Altitude and Eccentricity

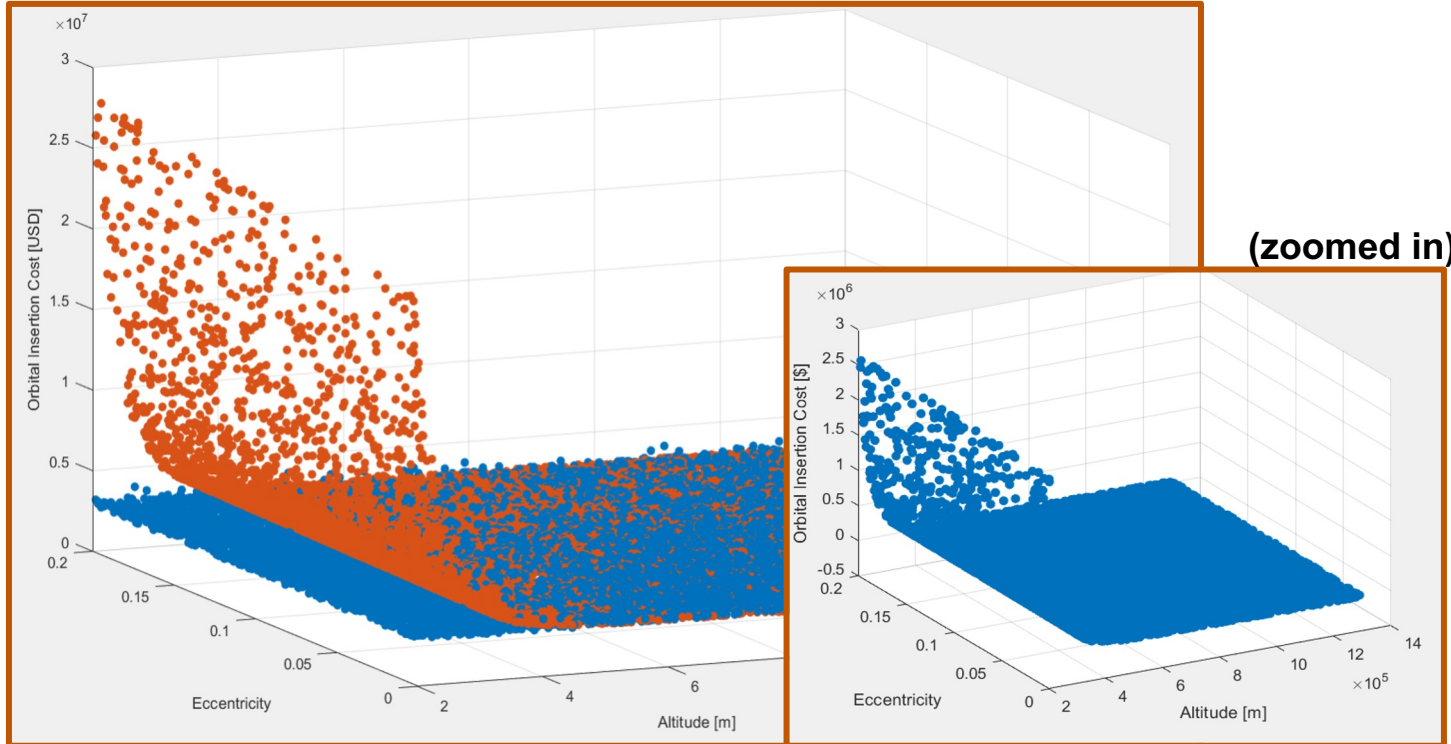


Figure 8

Mission Cost: 2D View

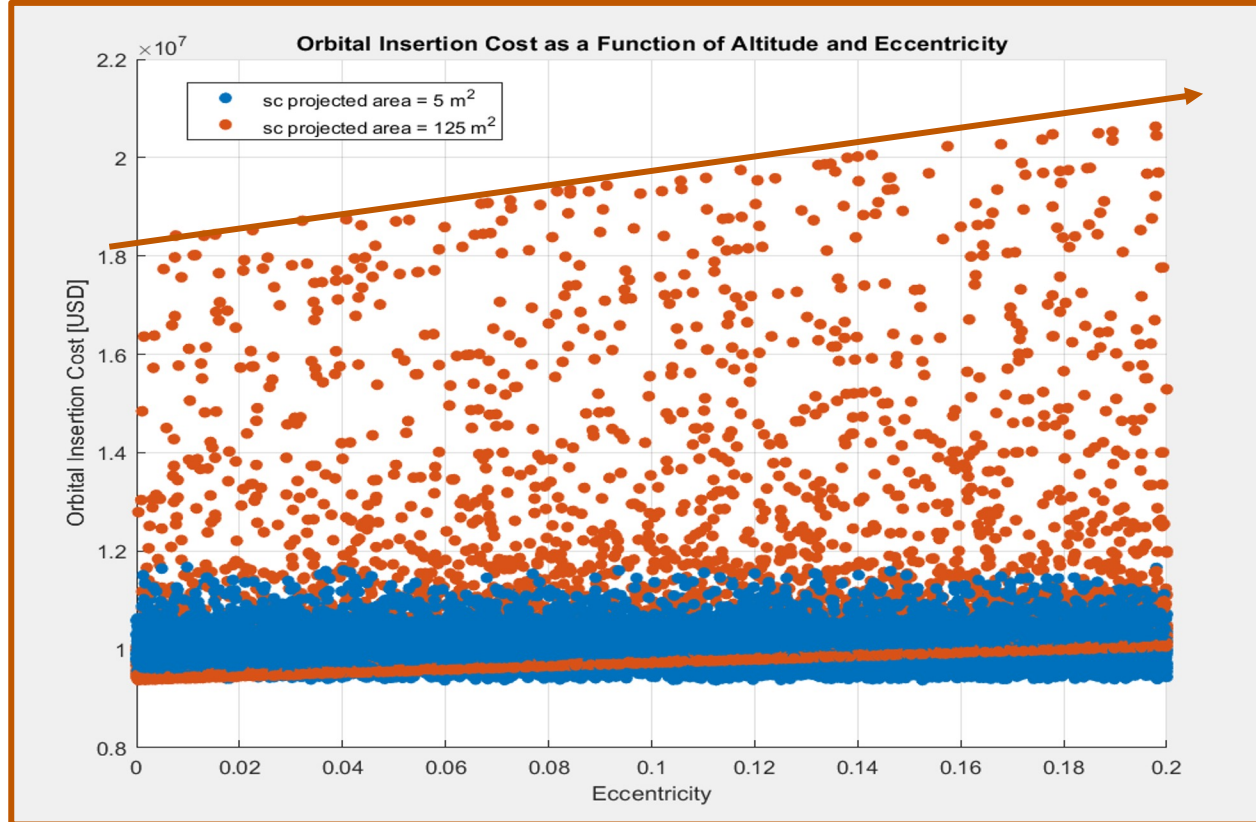


Figure 9:

Results Continued

Spacecraft Projected Area [m ²]	5	25	125
Optimal Orbital Altitude [km]	301	377	461
Optimal Eccentricity	~0	~0	~0
Total Projected Cost [Billions of USD]	9.38	9.73	9.94

Orbital Inclination Determination - Oblateness Perturbations

- Precession of the **ascending node**, Ω , due to J_2 .

$$\frac{d\Omega}{dt} = \frac{-3}{2} \cdot J_2 \cdot \left(\frac{R_E}{a(1-e^2)} \right)^2 \cdot \sqrt{\frac{\mu_E}{a^3}} \cdot \cos(i)$$

- Critical **inclinations** of **63.43 or 116.57 deg** minimizes perturbative effects [58].
- The delta-v required for an inclination change of 5.99 deg, as necessary for a launch from the Pacific Spaceport Complex, is 801 m/s.

Altitude Required for Repeating Ground Tracks

$$a_{RGT} = \mu^{1/3} \left(\frac{M}{N\omega_B} \right)^{2/3}$$

a_{RGT} = Orbital Radius

μ = Gravitational Parameter

M = # of Rotations of Earth

N = # of Spacecraft Revolutions

ω_B = Rotational Sidereal Frequency [1/s]

Summary: Resulting Orbit and Targeted Customers

Plots of Orbital Trajectory

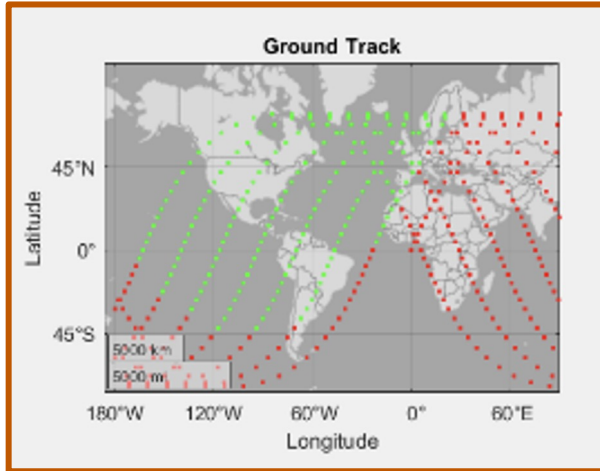


Figure 10

1. Altitude: 404 km.
2. Eccentricity: 0.
3. Inclination: 63.43.
4. Longitude of the ascending node (LAN) contingent on specific customer's location.
5. Repeat period: 2 days.
6. Launch site: Pacific Spaceport Launch Complex (latitude: 57 deg.).

Off-the grid Canadian communities host more than 200,000 people.

- Whitehorse (latitude: 60.72 deg N).
- Yellowknife (62.45 deg N).
- Arviat (latitude: 61.1078 deg N).

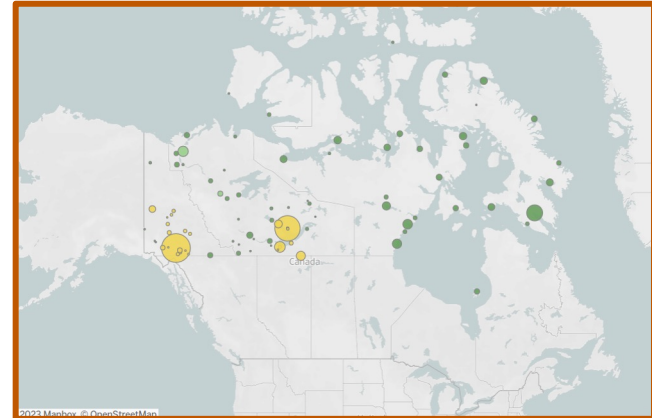


Figure 11: Map of Off-the-Grid Canadian Communities [27]

Upper Atmosphere Gas Dynamic Drag - Monte Carlo Analysis at 400 km

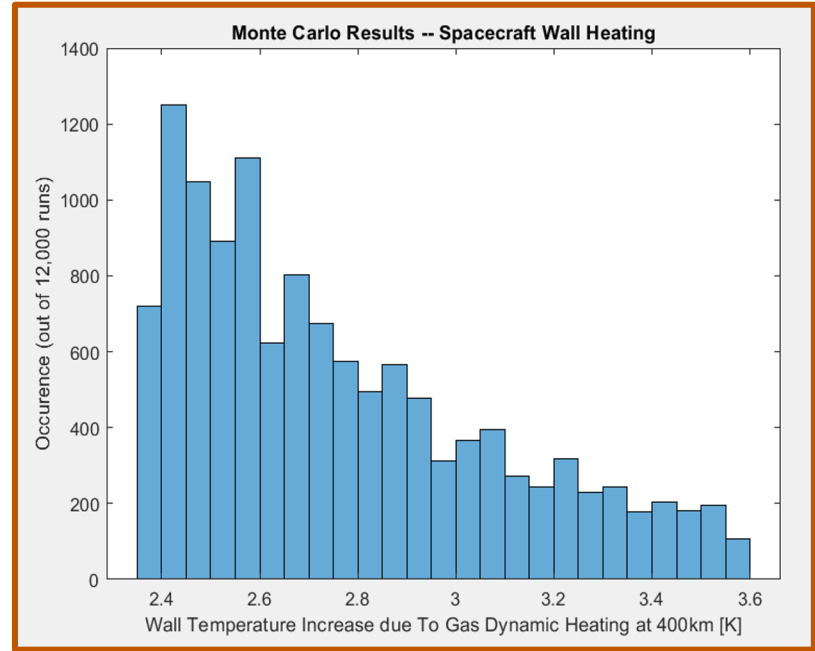
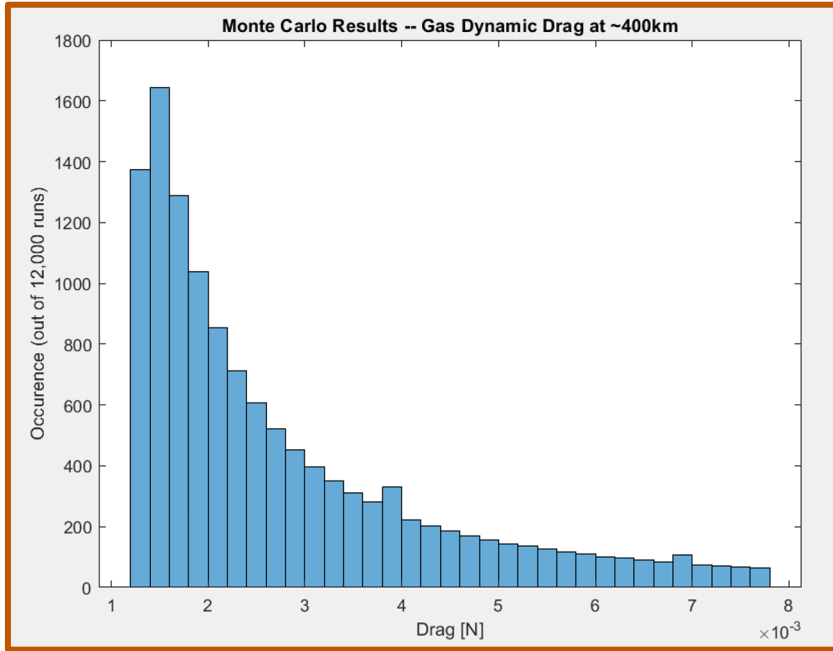


Figure 12 [3, 37].

Optimal Propulsion Engine Given Altitude

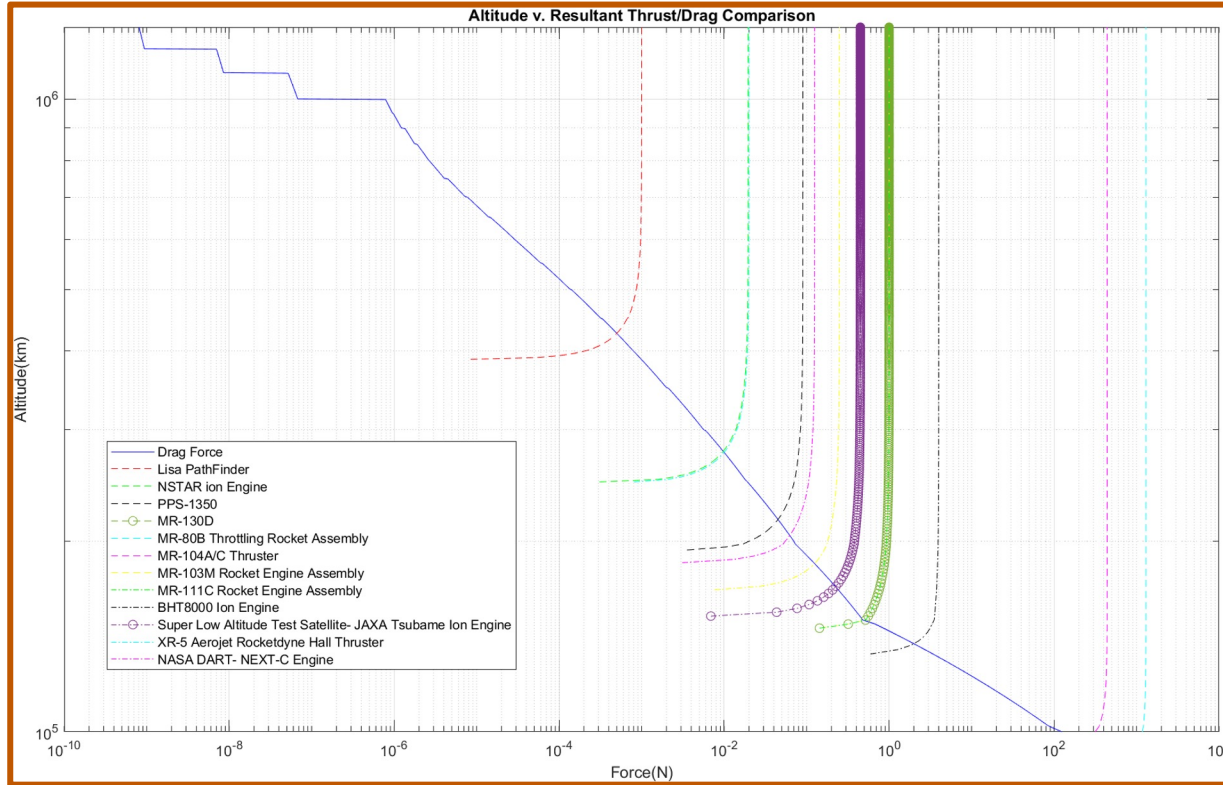


Figure 13

Thank You! | Questions?

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